

Application of Cardiovascular Models in Comparative Physiology and Blood Pressure Variability*

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Abstract—The usefulness of cardiovascular models is determined by their intended function with respect to elucidating underlying hemodynamic concepts and to enable simulations that will assist in understanding the effects of specific parameters. Models can take different forms, including mock circulatory constructs with physical components, mathematical representations of parameter space relations employing constitutive equations, or closed form representations of electrical circuit analogs described in the time or frequency domain. This investigation describes the use of cardiovascular models based on electrical analogs of mechanical hydrodynamic systems to elucidate two different physiologic concepts: (i) the use of distributed vascular impedance to investigate comparative physiology of optimal design and features related to body size across a broad range of animal species; (ii) use of lumped parameter models to assess the role of arterial stiffness in blood pressure variability. The impedance model shows that an allometric relationship between body weight and aortic effective length can be determined by using the frequency of minimum input impedance and aortic pulse wave velocity. This concept provides a background for optimal matching of body size and hemodynamic load on the heart. The lumped parameter model indicates that arterial stiffness, simulated by the total arterial compliance term, has a significant impact on variability of arterial pressure when changes are due to dynamic alterations of peripheral resistance. In addition, the known pressure dependency of arterial stiffness results in a curvilinear relationship between blood pressure variability and mean pressure. This has implications in hypertensive treatment where there are marked changes in arterial stiffness, as occurs with aging.

I. INTRODUCTION

Early studies in hemodynamics were aimed at reducing the complexities of the fluid dynamic problem of blood flow in arteries so as to be able to compute flow velocity from the measurable pressure gradient [1], [2]. This led to the broader consideration of the relatively small effects of the non-linear properties [3] so that the relationship between pulsatile arterial pressure and flow can be described by the concept of the electrical analogy of impedance, a quantity described in the frequency domain [1]. When the relationship is determined as input impedance of the systemic and pulmonary arterial trees, it becomes the complete description of the hydraulic load on the ejecting ventricles. The impedance concept, such that it can be described by physical elements,

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advanced the modeling of hemodynamic phenomena and lead to implementation of physical and mathematic models to describe the underlying concepts of arterial design [4]–[9].

This paper aims to present the use of models that are based on the impedance concepts to illustrate their use in describing the pulsatile arterial load and to assess fundamental quantities of arterial design over a large range of animals of body size as well as quantifying the effect of a fundamental arterial property, arterial stiffness, on the dynamic variability of arterial pressure.

II. ARTERIAL IMPEDANCE

A. Calculation of impedance spectra

Impedance is defined in the frequency domain and relates oscillatory components of the time-varying signals of pressure, $P(t)$ and flow $Q(t)$. Assuming that $P(t)$ and $Q(t)$ are periodic functions and the system is stationary, the harmonic components, $P_k(\omega)$ and $Q_k(\omega)$ are obtained by Fourier decomposition of $P(t)$ and $Q(t)$ and the impedance spectrum is calculated (1).

$$Z_k(\omega) = \frac{P_k(\omega)}{Q_k(\omega)}; \quad (k = 1, 2, \dots, N) \quad (1)$$

This is a complex quantity with modulus ($|Z|_k(\omega)$) and phase ($Z_{phs}_k(\omega)$) plotted as function of frequency for the N harmonics. For physiological signals the impedance spectrum can be completely specified for $N = 10$.

Fig 1 shows aortic impedance in two animals, rabbit and guinea pig, with markedly different body size. Both show a frequency of impedance minimum and phase zero crossing, but the smaller size guinea pig (and higher heart rate (HR)) is at a higher frequency (10-11 Hz) compared to the rabbit (5-6 Hz). From this spectrum, association with single tube behavior led to considerations of arterial effective length (L_{eff}), determined from the ‘resonance’ frequency of minimum impedance modulus (f_{min}) and the pulse wave velocity (c) by equating it to a quarter wavelength ($L_{eff} = c/(4 \cdot f_{min})$) [6], [10]–[12].

This concept was used in comparing impedance spectra across a range of species of different body size (Fig 2, Table I).

B. Allometric relations

The allometric concepts employed in scaling laws [17]–[20] were used to assess whether an invariant relation exists between L_{eff} and body weight (2), where c is a scalar quantity and k is the power exponent.

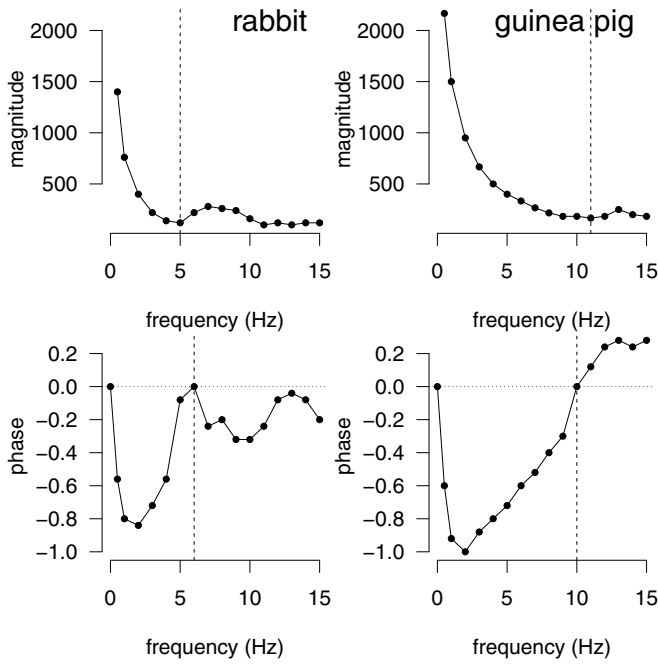


Fig. 1. Input impedance in rabbit and guinea pig [13], [14], showing a higher frequency for the minima of magnitude and phase zero crossing (dashed lines) for the lower body weight animal (rabbit).

TABLE I

ALLOMETRIC SCALING DATA FOR VARIOUS ANIMAL SPECIES ACROSS A RANGE OF BODY WEIGHTS.

species	weight (kg)	HR (Hz)	PWV (cm·s ⁻¹)	f_{min} (Hz)	L_{eff} (cm)
rat	0.45	5.8	600	14.0	10.7
guinea pig	0.70	3.9	480	14.0	10.0
rabbit	3.0	3.5	450	4.5	25
snake	5.6	0.67	593	3.0	49
dog	5.8	2.4	590	4.0	31
kangaroo	23.3	1.4	469	2.5	47
sheep	33	2.1	520	2.0	65
human	72	1.2	600	3.5	43

$$\log(L_{eff}) = k \cdot \log(\text{body weight}) + c \quad (2)$$

From the data in Table I, the relationship is shown in Fig. 3, with a high correlation, indicating that the known allometric parameters related to body size in terms of optimizing metabolism [17], [18] are also relevant with respect to matching of arterial impedance to ventricular ejection, since they were determined from the frequencies corresponding to impedance minima.

III. LUMPED PARAMETER MODEL

A. Circuit components

The systemic arteries are represented by a 4-element windkessel model with the equivalent circuit elements of aortic characteristic impedance (Z_c), blood inertia (L), total peripheral resistance (TPR) and aortic compliance (C), which is also a function of pressure ($C(P)$) (Fig. 4). The nominal values for the circuit elements are: Z_c : 0.05

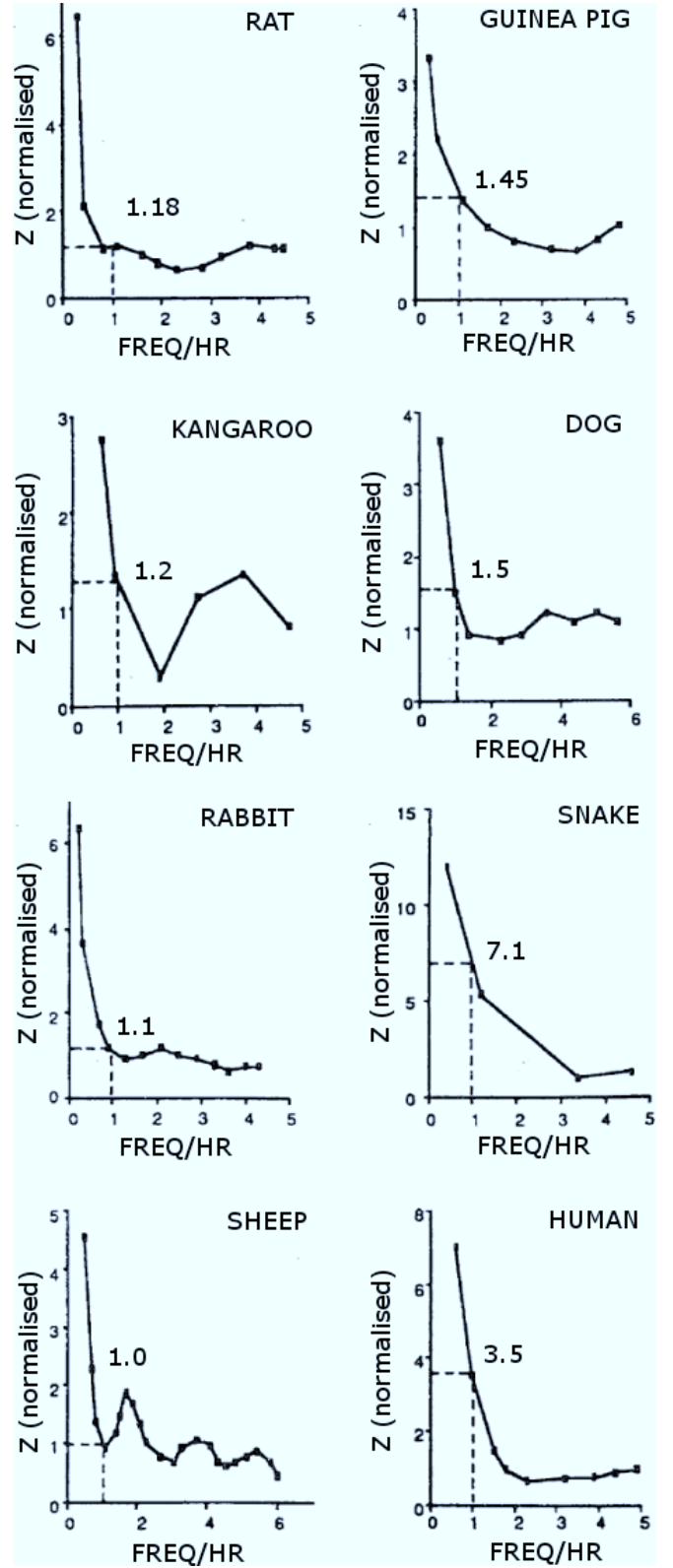


Fig. 2. Impedance modulus normalised for characteristic impedance and resting HR for each species. The figure indicates the normalized modulus value at the equivalent resting HR. Note that some mammalian species (human) have a comparatively higher relative impedance at the normal HR, indicating reduced matching based on allometric data (Fig. 3) (Data obtained from previous studies [4], [13]–[16]).

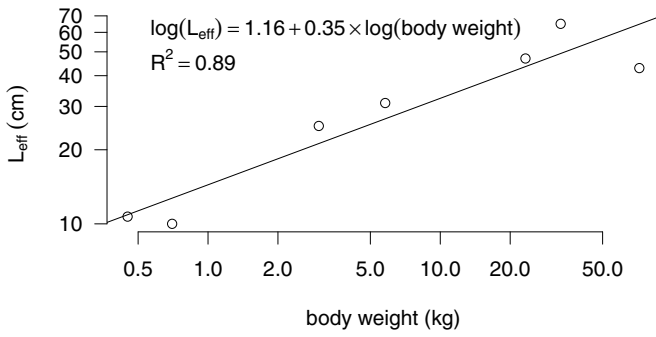


Fig. 3. Allometric relationship between aortic effective length (L_{eff}) and body weight determined for mammalian species (ie. snake not included), as per Table I, expressed on log axes.

mmHg·m⁻¹·s; L : 0.008 mmHg·ml⁻¹·s²; C : 2 ml·mmHg⁻¹; TPR: 1.2 mmHg·ml⁻¹·s.

The input to the model is a physiological flow wave at a nominal HR of 60 beats/min. All simulations were performed in Simulink and Matlab.

IV. SIMULATION OF BLOOD PRESSURE VARIABILITY

A. Blood pressure variability index

The importance of blood pressure variability (BP_v) is being increasingly recognized with evidence emerging of the association of BP_v with cardiovascular risk, independent of average levels of BP [21]. In addition, BP_v has also been shown to be associated with large artery stiffness, as measured by pulse wave velocity [22].

For this analysis, the index for BP_v , SBP_v (%), was determined from the standard deviation (SD) and mean of systolic pressure (SBP_m) over 5 minute epochs (3).

$$SBP_v(\%) = 100 \cdot \frac{SD}{SBP_m} \quad (3)$$

B. Variation of peripheral resistance

The variation in blood pressure is brought about by variation in TPR or in stroke volume. For variation in TPR, a random function is generated with a Gaussian distribution such that the value (TPR_v) varies randomly around a constant value (TPR_c) beat-to-beat (4). The random generator function uses real constants (a and c) and a seed value (x).

$$TPR_v = a \cdot \exp\left[\frac{-(x - TPR_c)^2}{2c^2}\right] \quad (4)$$

C. Pressure dependency of arterial compliance

The pressure dependency of the stiffness of the arterial wall is modeled by assigning an exponential relation between aortic compliance (C) and mean BP (MBP), using a constant (k) that varies with age [23] (eg. 0.022, 0.016, 0.07 for ages 30, 50 and 80 years respectively), and a constant compliance coefficient (C_0) (5).

$$C = C_0 \cdot \exp(-k \cdot MBP) \quad (5)$$

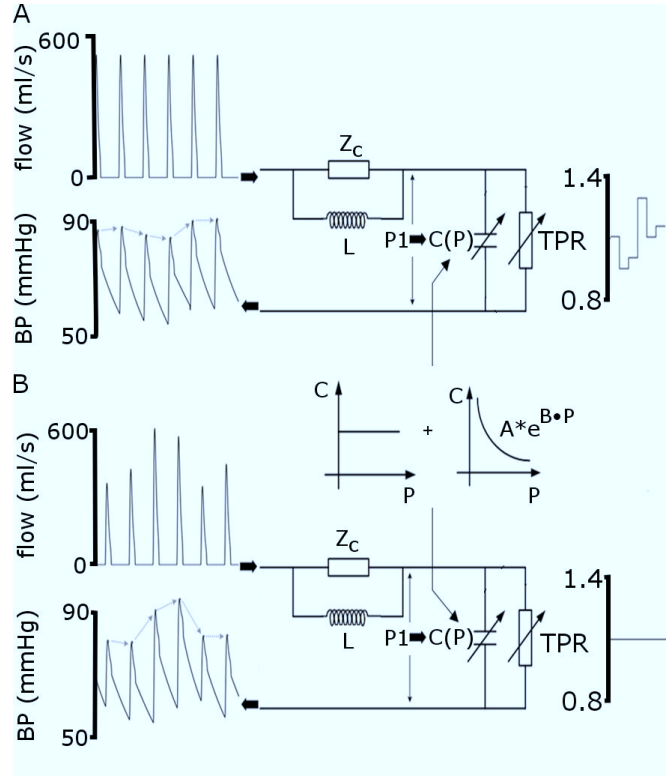


Fig. 4. Circuit representation of a 4-element Windkessel model: aortic characteristic impedance (Z_c), blood inertia (L), TPR and aortic compliance (C), which is also a function of pressure ($C(P)$), the exponential relation shown in the center. A. The flow input is constant (upper trace) and the blood pressure (lower trace) varies due to randomly varying value of TPR (right). B. TPR is constant and blood pressure (lower trace) varies due to variation in stroke volume (upper trace).

D. Characterization of blood pressure variability

Simulations were conducted using the model to quantify the relation between SBP_v (%) and the causal variable for variability in BP. Fig. 5 shows SBP_v (%) when variability is due to random variation in TPR using 5 min epochs at varying values of mean TPR, for pressure independent and pressure dependent arterial compliance. Since when TPR is varied, stroke volume (SV) and HR are constant, the change in TPR is proportional to mean BP.

The random variation in TPR (simulating neurogenic activity) resulting in BP_v has different effects for pressure dependent and pressure independent compliance. For constant compliance, BP_v decreases with increasing mean BP, but with pressure dependent compliance, the relationship is curvilinear, indicating an ‘optimal’ value of mean BP where BP_v is minimal.

V. DISCUSSION

The models presented in this paper illustrate the potential for closed form representation of the arterial system to investigate underlying concepts ranging from evolutionary adaptations for optimal cardiovascular function to effects of basic parameters on dynamic changes in blood pressure. Comparative physiology allows investigations of fundamental laws governing physiological function [12]. The

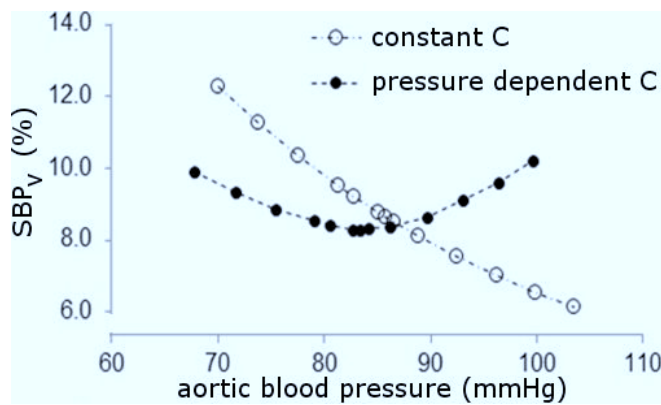


Fig. 5. Blood pressure variability index (SBP_v (%)) as a function of mean aortic blood pressure for a constant (pressure independent) compliance and for a pressure dependent compliance.

impedance concepts using distributed models [24] uncover possible maladaptive changes across animal species. For example, the human arterial system has a relatively higher impedance, and so pulsatile load at the normal cardiac frequency compared to other species.

Lumped parameter models enable implementation of realistic hemodynamic load for cardiac experimentation [25]. Our recent simulations on the effects of arterial stiffness on BP_v has illustrated a further optimal function where a given value of mean pressure exists for minimal variability in systolic pressure, for a given variability in peripheral resistance. This has significant implications in the optimization of anti-hypertensive treatment. Currently, hypertension guidelines recommend similar BP targets for all age groups [26]. However, given the known decrease in pressure dependency of arterial stiffness with age [23], the optimal value of blood pressure for minimal variability would not be similar across ages. And this may be one of the explanations for different risk profiles among treated hypertensives, given the increasing importance of BP_v in cardiovascular risk [27].

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